

# Influence of Vanadium Microalloying on the Microstructure of Induction Hardened 1045 Steel Shafts

---

*Lee M. Rothleutner, The Timken Company*

*Chester J. Van Tyne, Colo. School of Mines*

*Robert Goldstein, Fluxtrol Inc.*

**TIMKEN**

**ASPPRC** Advanced Steel Processing  
& Products Research Center  
 **COLORADO SCHOOL OF MINES**  
EARTH • ENERGY • ENVIRONMENT

 **FLUXTROL**  
Centre for Induction Technology.

*With Additional  
Support From*

 **GERDAU**

**FCA**  
FIAT CHRYSLER AUTOMOBILES

**NORTH  
AMERICA**

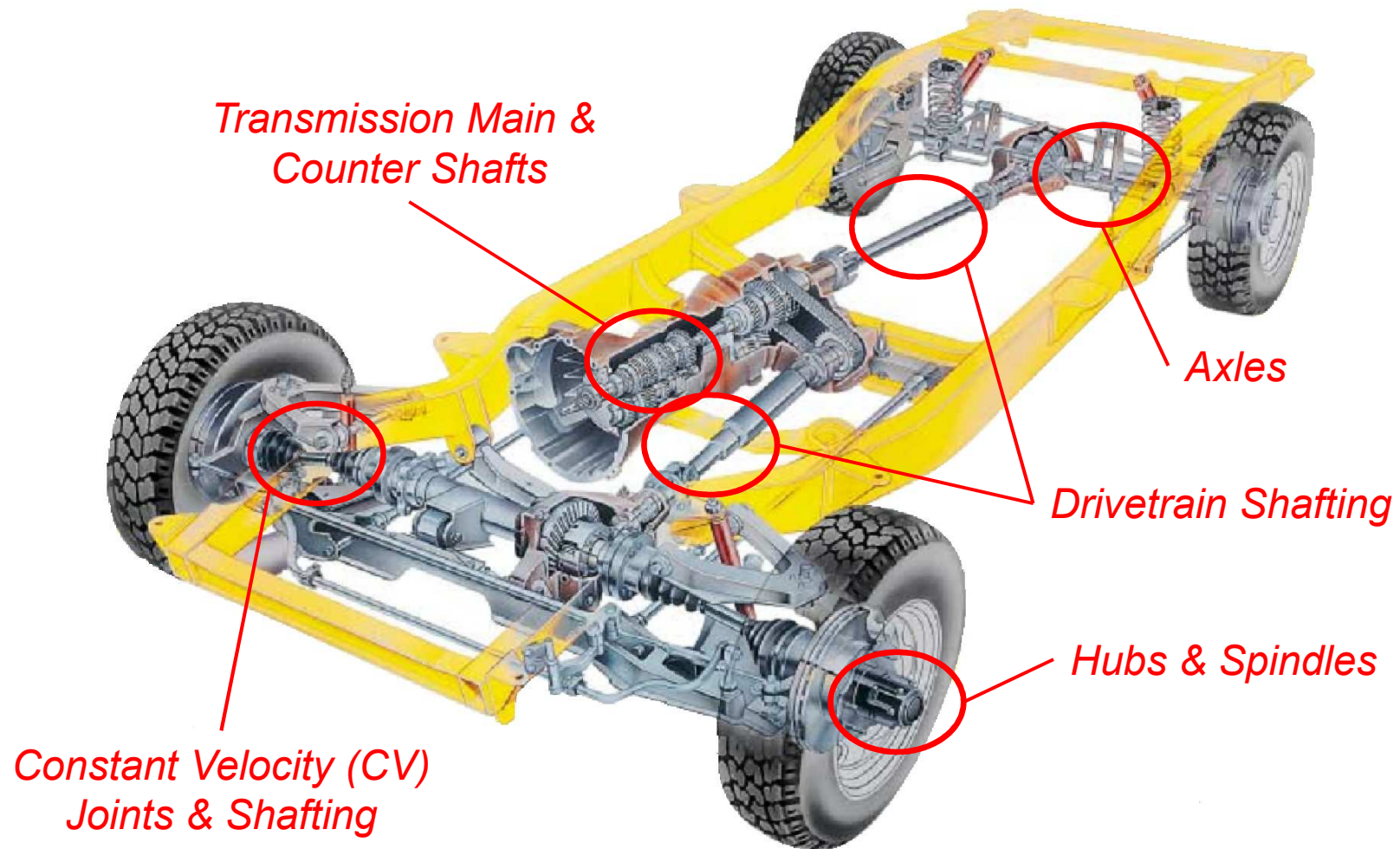
 **INDUCTOHEAT**  
An Inductotherm Group Company

 **HTS**  
Heat Treating Society  
ASM INTERNATIONAL

 **ASM**  
INTERNATIONAL

# Motivation

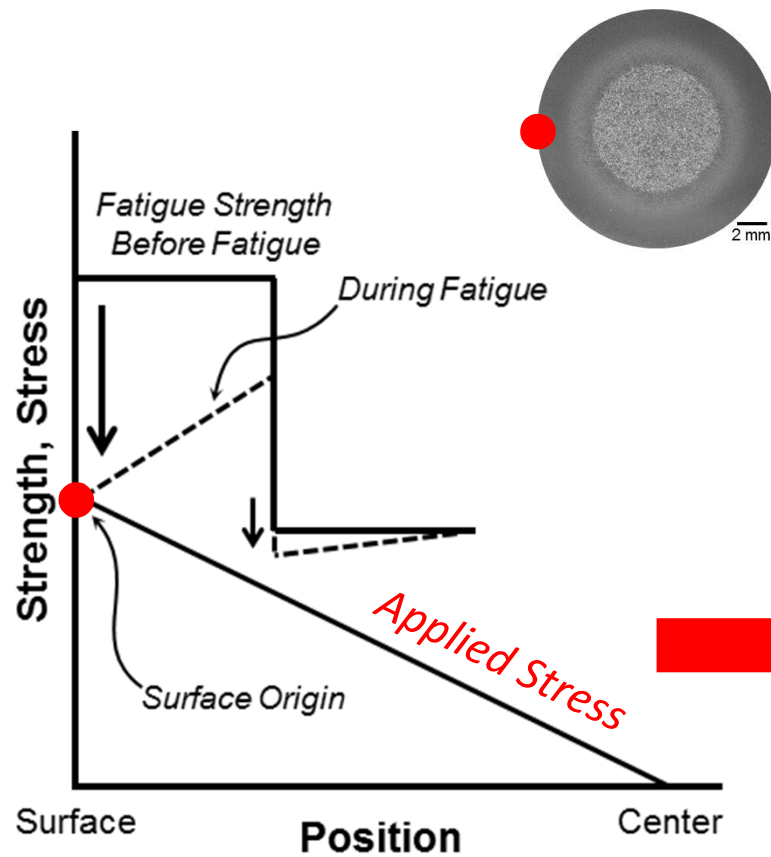
## *Applications of Induction Hardened Medium-carbon Steels*



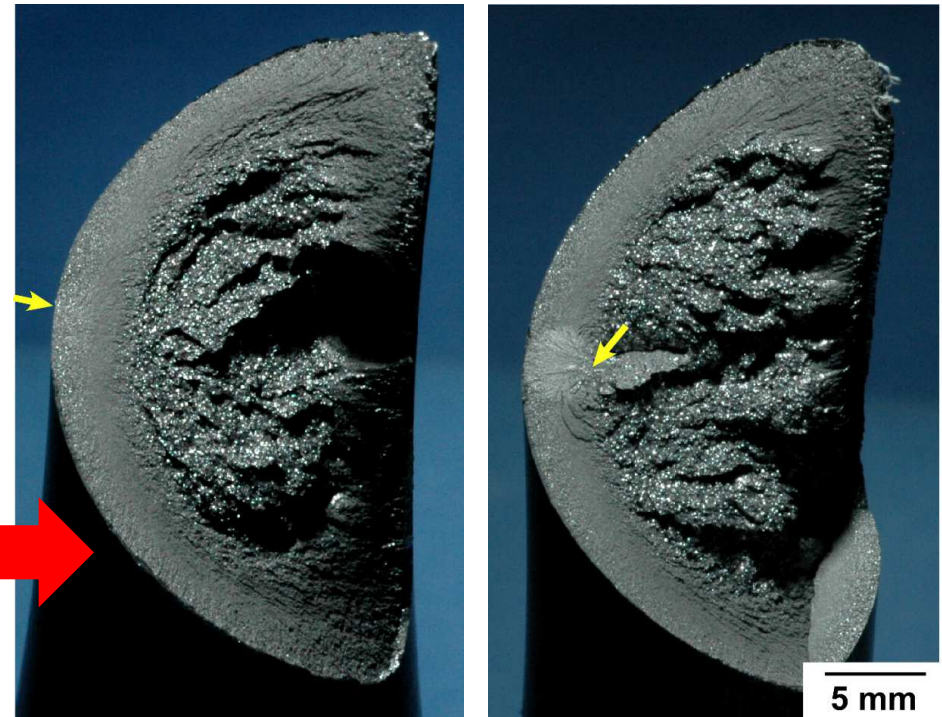
(Bayer, 2003)

# Motivation

Improving fatigue performance...



**Torsional Fatigue Failures**  
(550 MPa,  $R=0.1$ )



**Surface**

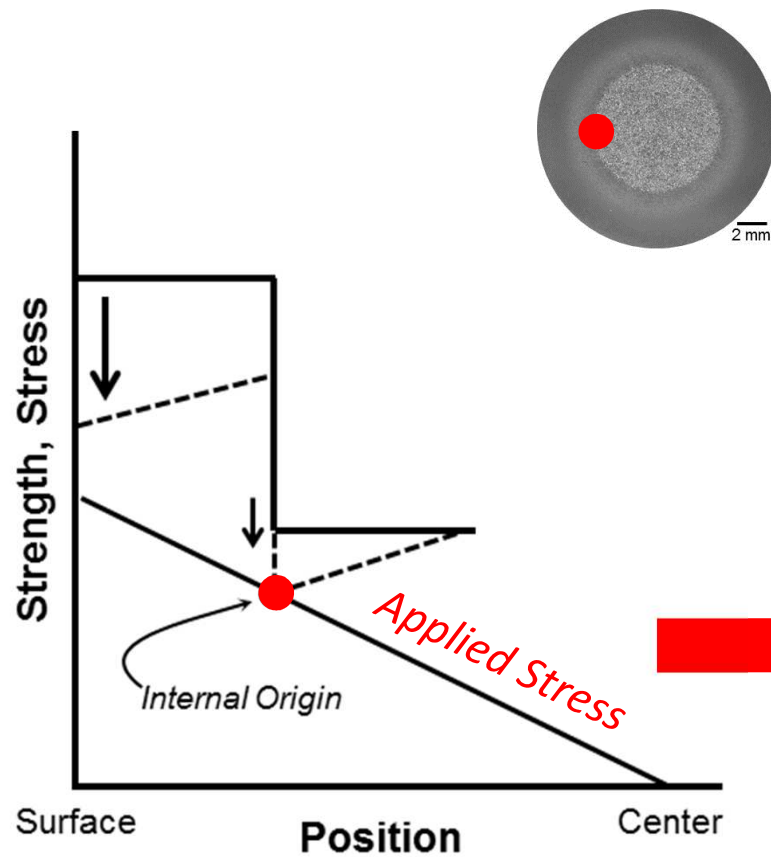
**Sub-surface**

(Ochi et al. 1999)

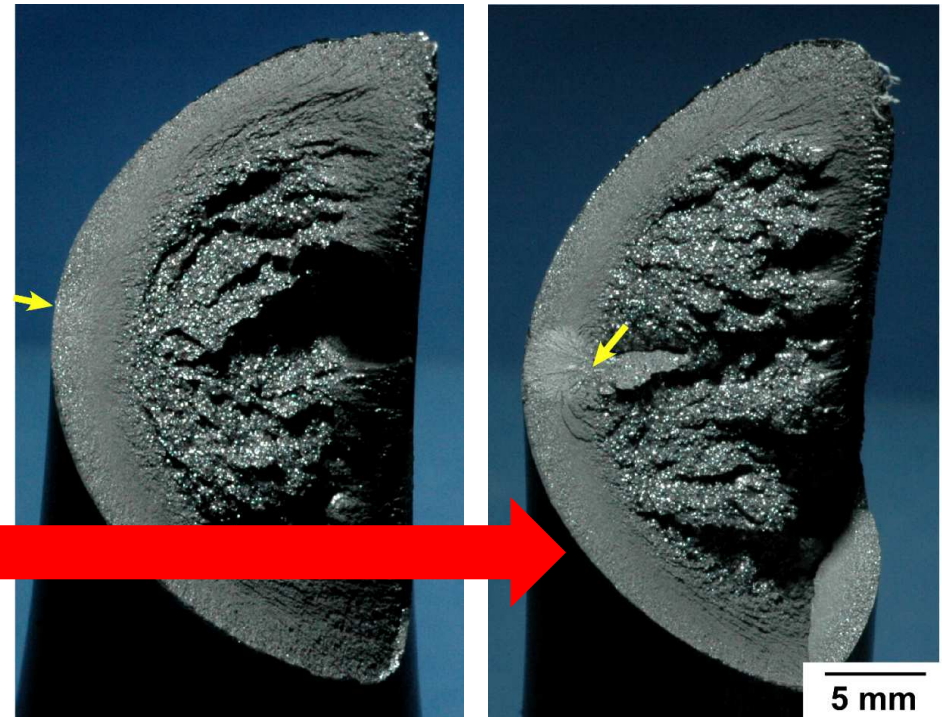
(Rothleutner et al. 2015)

# Motivation

Improving fatigue performance...



**Torsional Fatigue Failures**  
(550 MPa,  $R=0.1$ )



Surface

**Sub-surface**

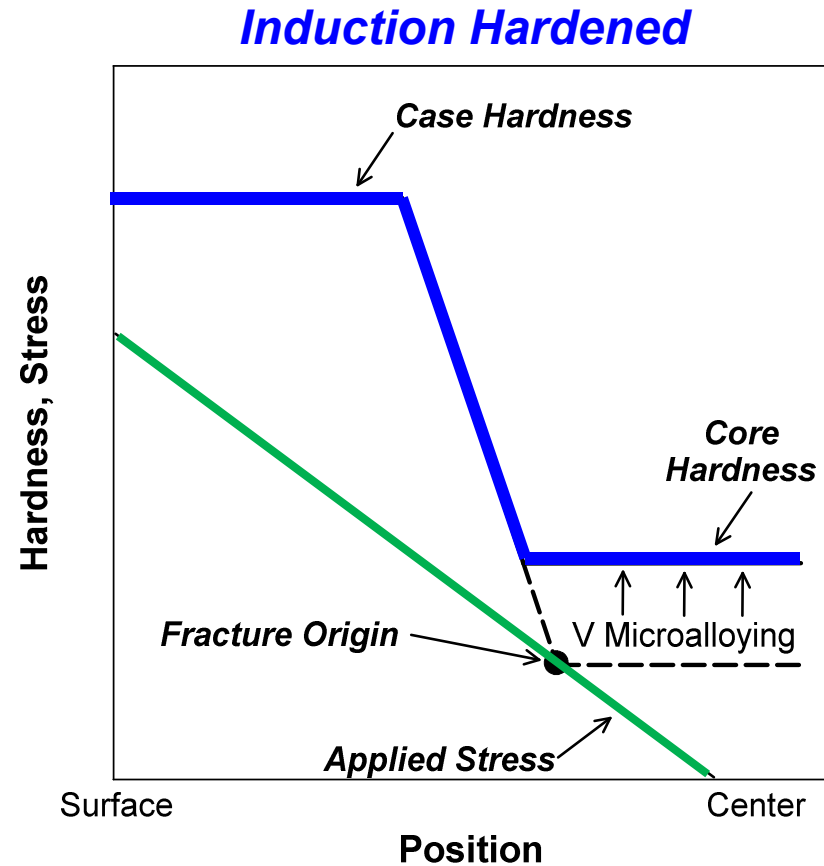
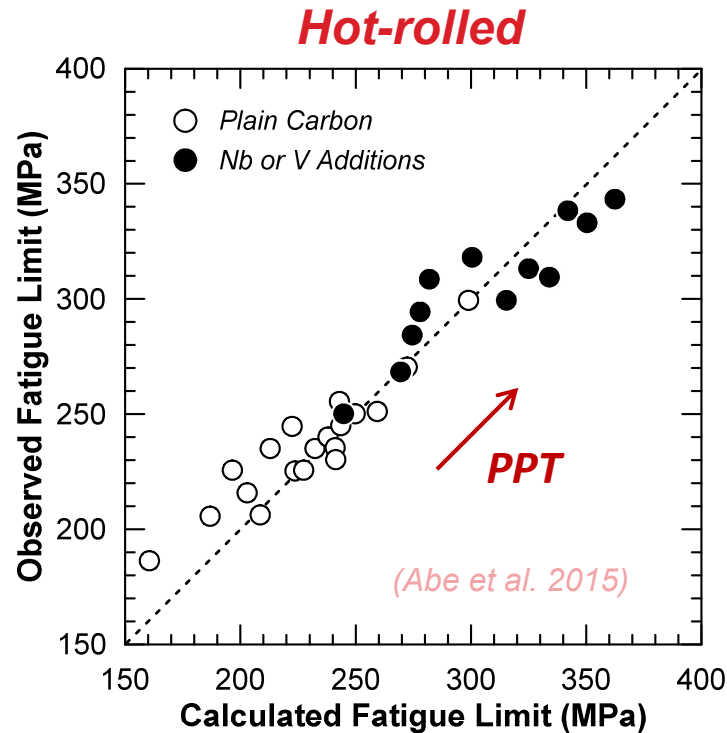
(Ochi et al. 1999)

(Rothleutner et al. 2015)



# Motivation

How will vanadium microalloying influence fatigue life?

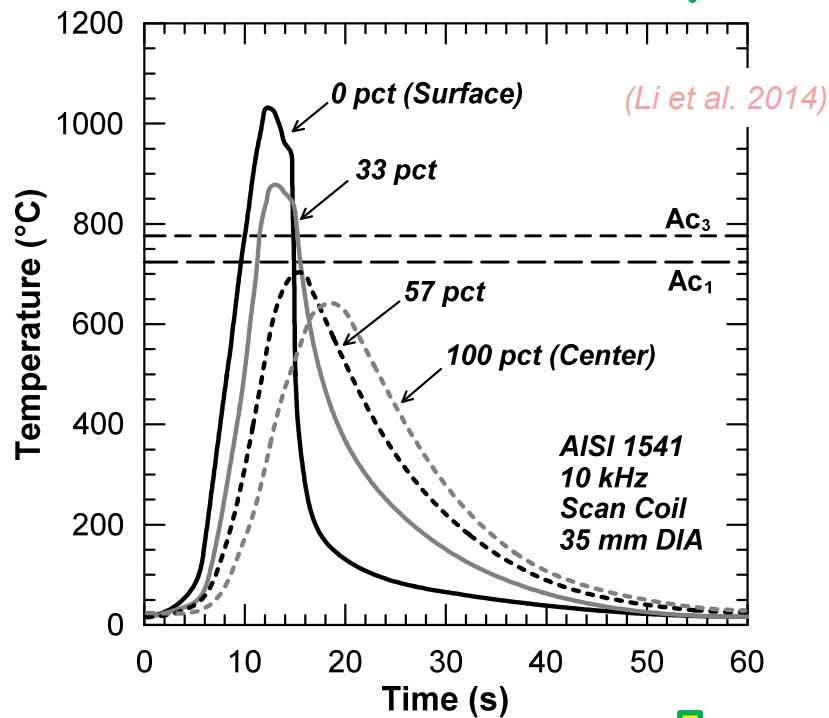


(Rothleutner, 2015)

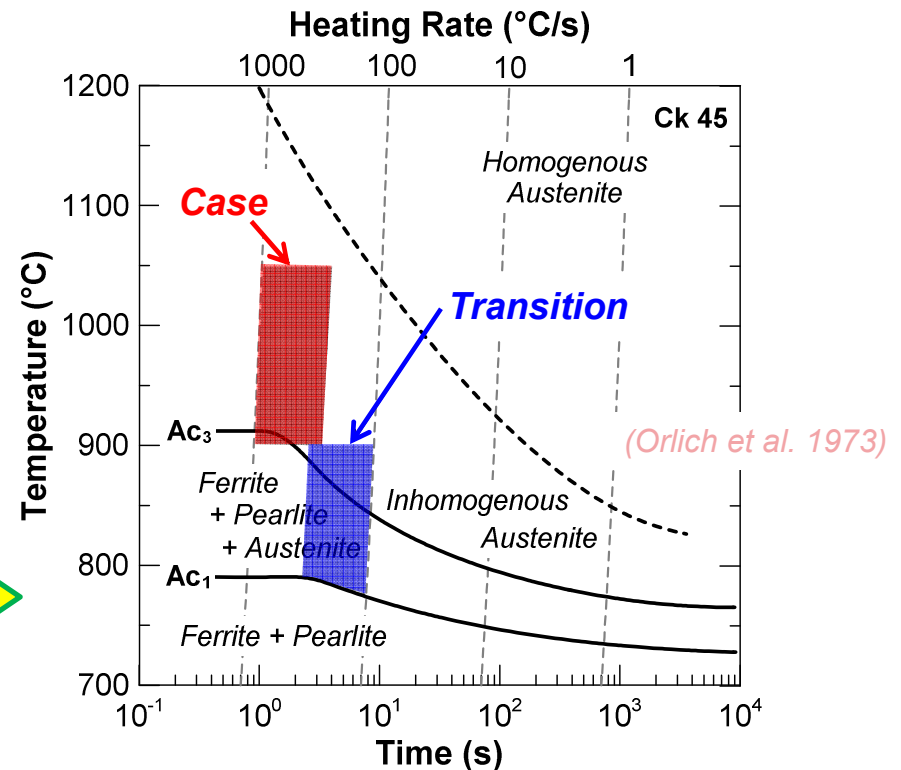
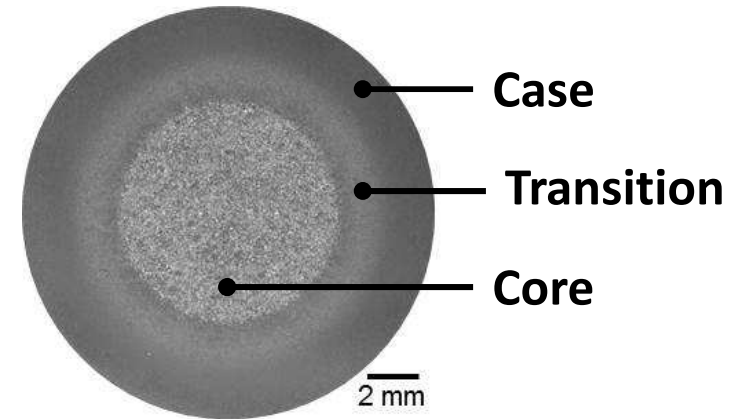
$$\sigma_w = 8.4 + 0.92 \sigma_{ss} + 0.70 \sigma_{ppt} + 0.53 \sigma_{prlt} + 0.43 \sigma_{gr} + 0.23 \sigma_{dis}$$

# Background

## Induction Hardening



Heating rate and peak temperature are a function of distance from center.

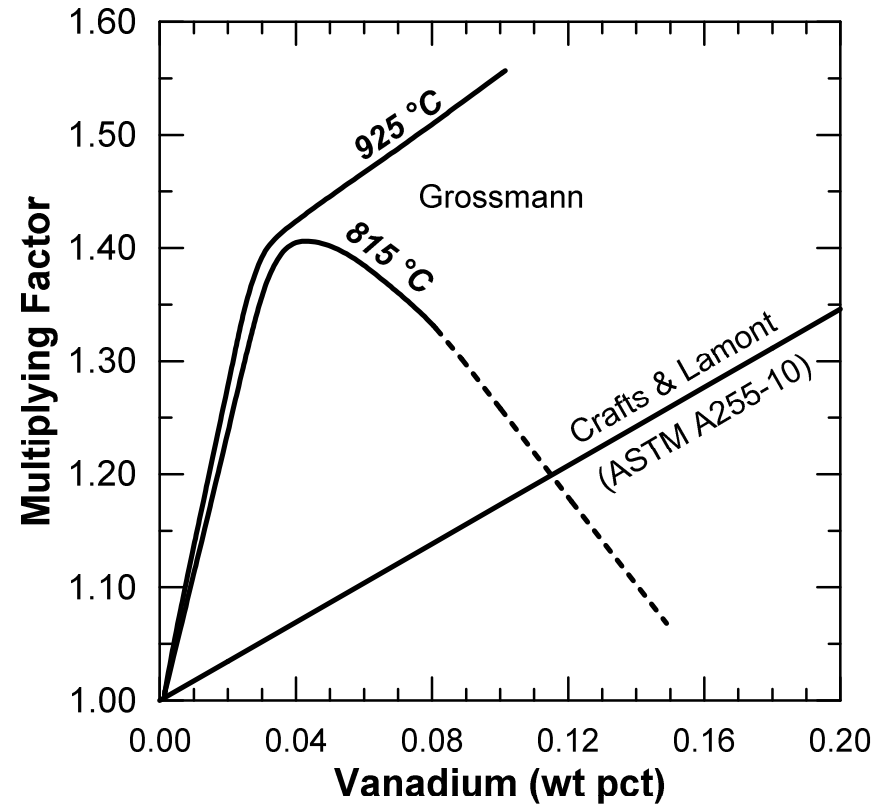


# Background

## *Effect of Vanadium on Hardenability*

Magnitude depends on state of vanadium in the steel.

- Precipitate vs. Solid-solution

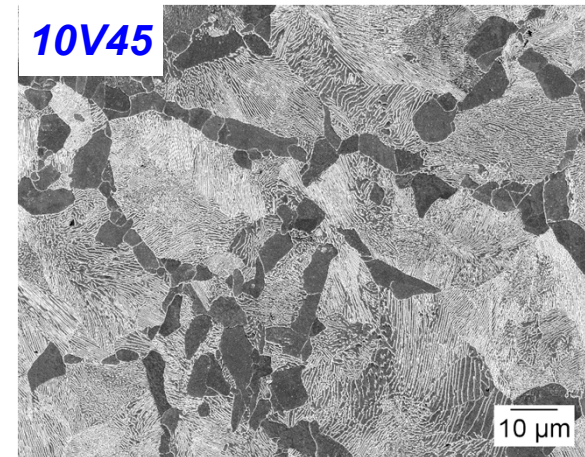
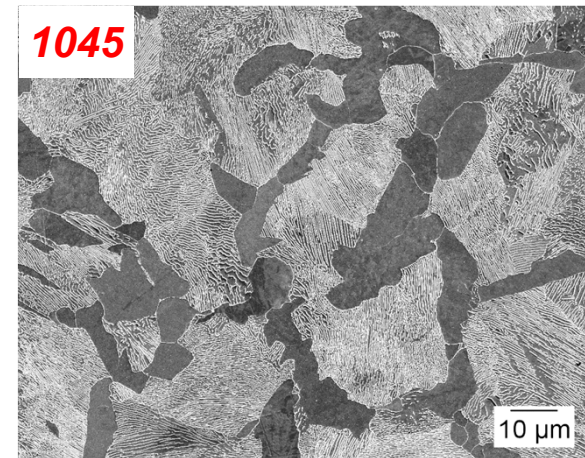


(Rothleutner, 2015)

# Materials

## Chemistry & Microstructure

8



	1045	10V45	$\Delta$ (pct)
Ferrite (%)	14.9 - 18.9	12.0 - 15.0	-25
Ferrite Grain Size ( $\mu\text{m}$ )	5.0 - 5.7	2.7 - 3.1	-85
Microhardness ( $\text{HV}_{1\text{kg}}$ )	$217 \pm 5$	$281 \pm 9$	+23

wt.%	C	Mn	Si	Ni+Cr+Mo	V	Al	N	P	S	Cu	DI <sup>a</sup> (mm)
1045	0.44	0.74	0.23	0.25	0.002	0.016	0.0068	0.010	0.006	0.26	35.6
10V45	0.47	0.82	0.28	0.24	0.080	0.007	0.0100	0.007	0.009	0.22	45.5

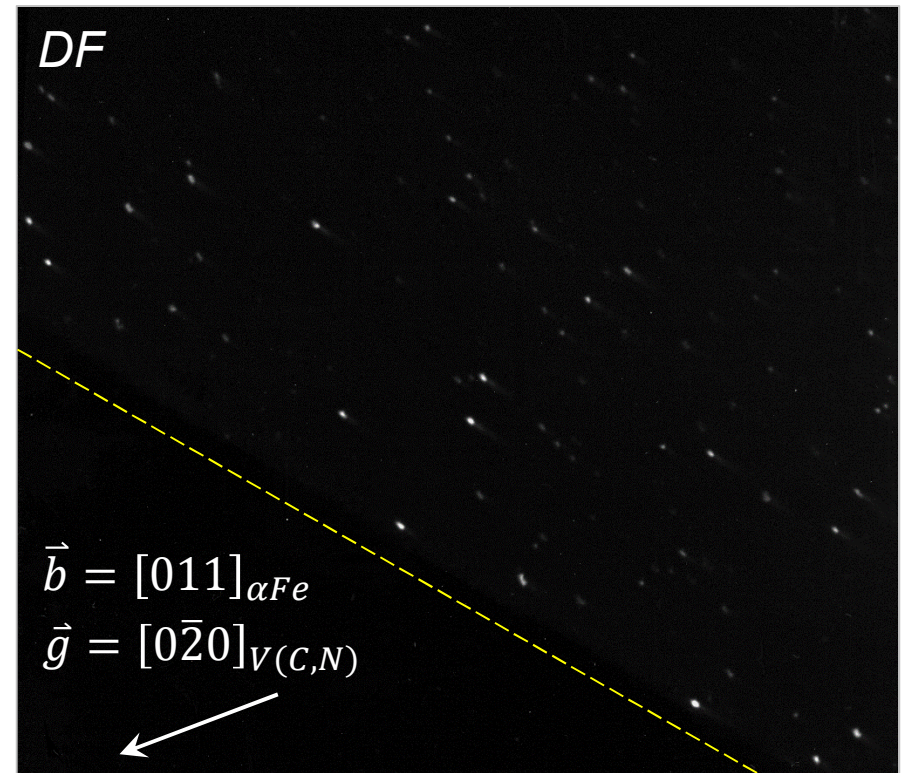
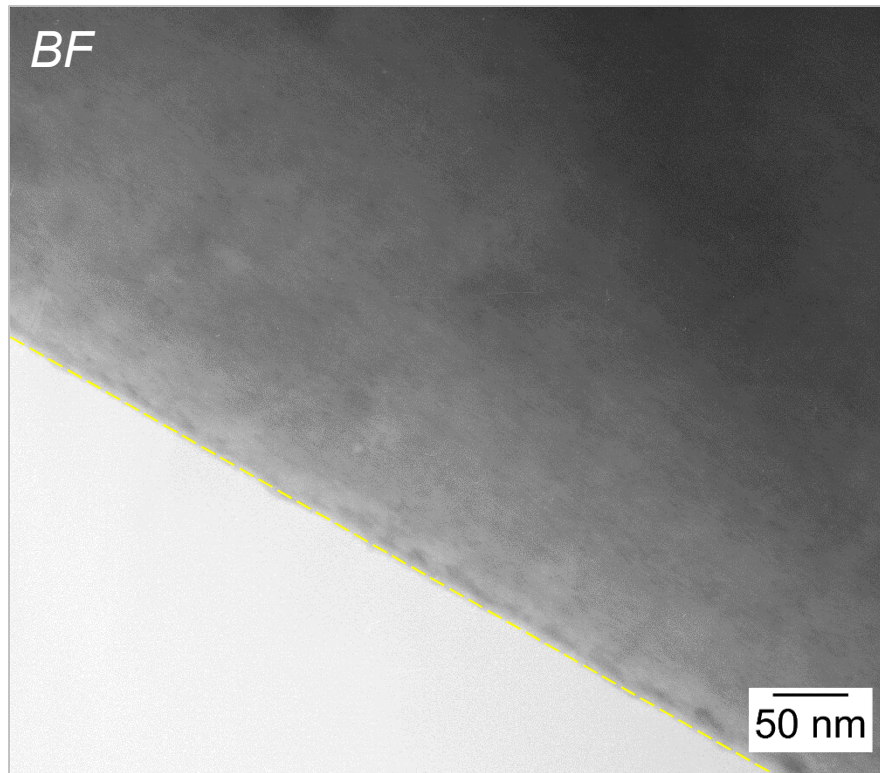
<sup>a</sup> ASTM A255-10: Standard Test Methods for Determining Hardenability of Steel



# Materials

9

## *V(C,N) Precipitation in 10V45 – Proeutectoid Ferrite*

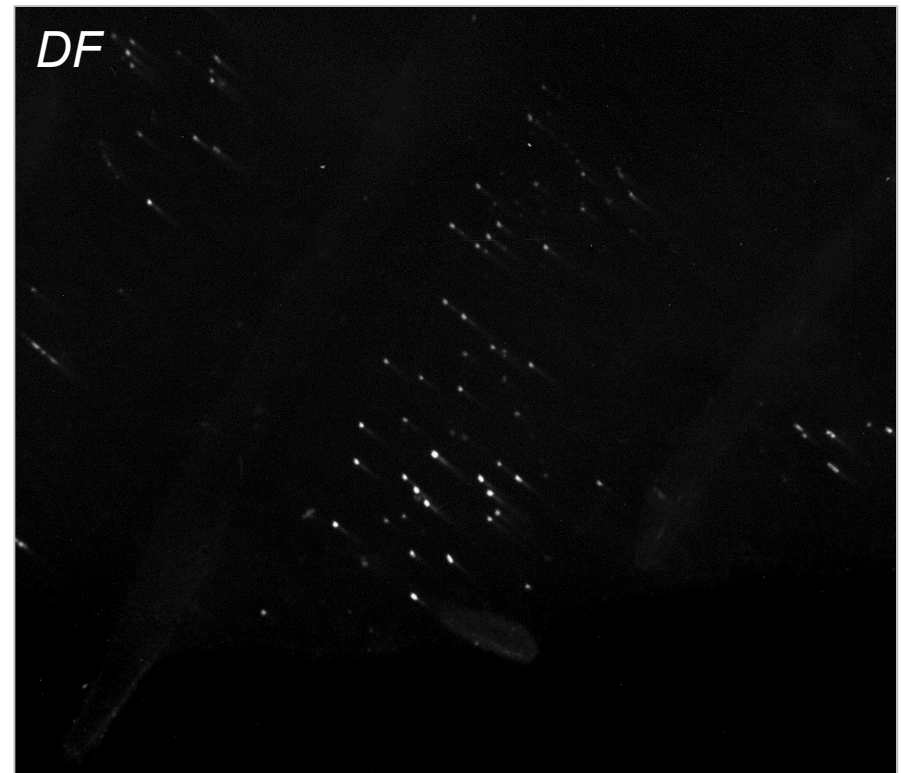
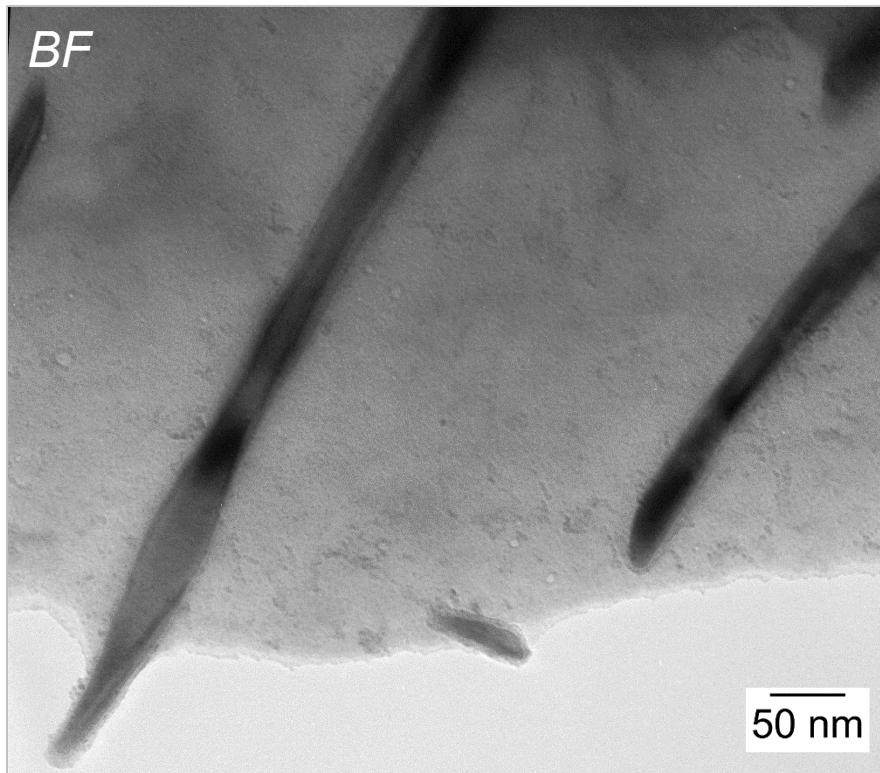


*V(C,N) diameter*  
 $4.5 \pm 0.3 \text{ nm}$

# Materials

10

*V(C,N) Precipitation in 10V45 – Pearlitic Ferrite*



*V(C,N) diameter*  
 $3.3 \pm 0.3 \text{ nm}$

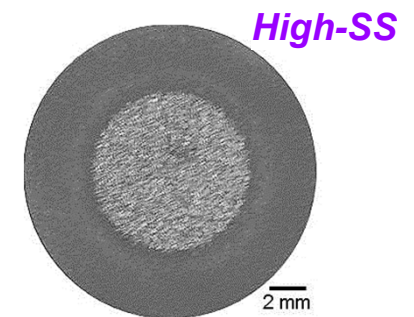
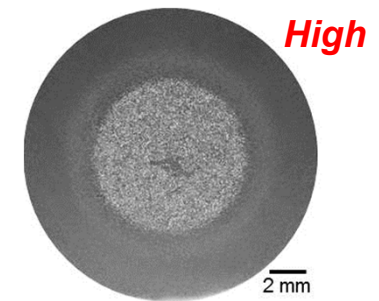
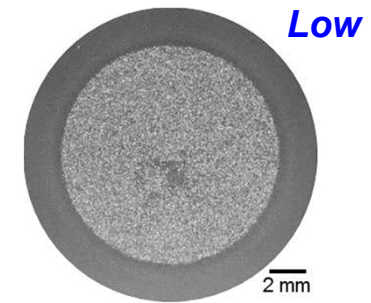
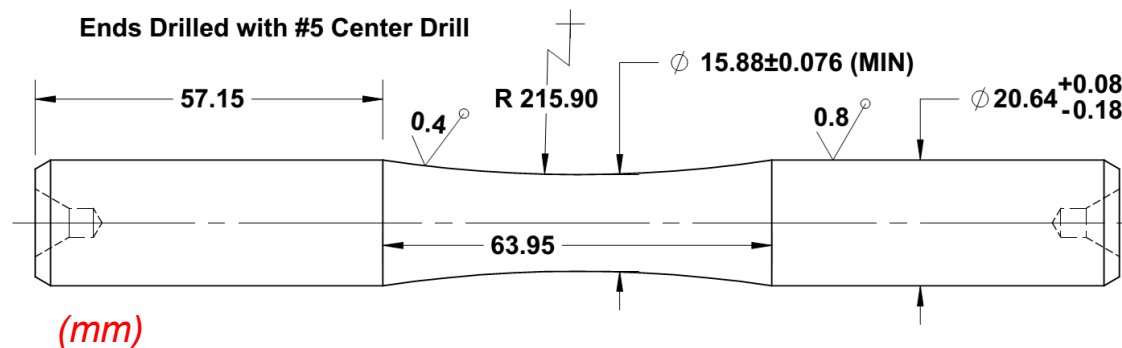


# Induction Hardening

11

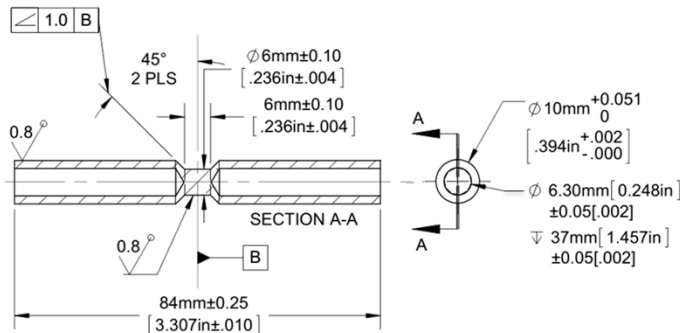
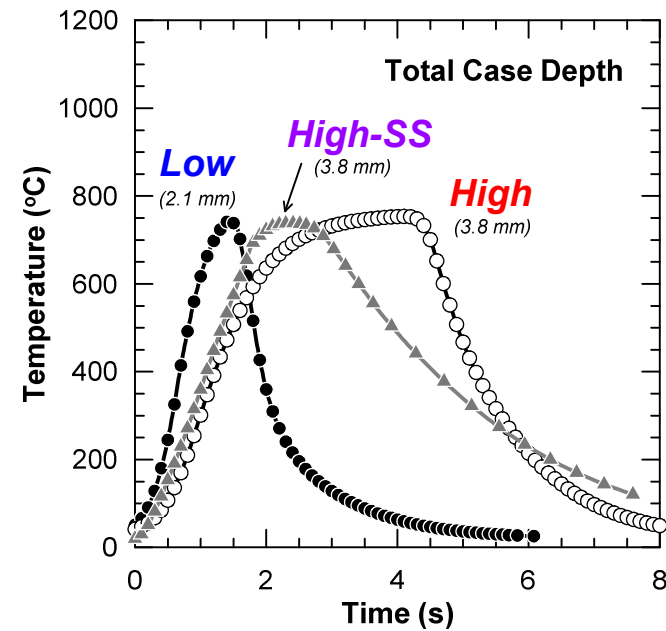
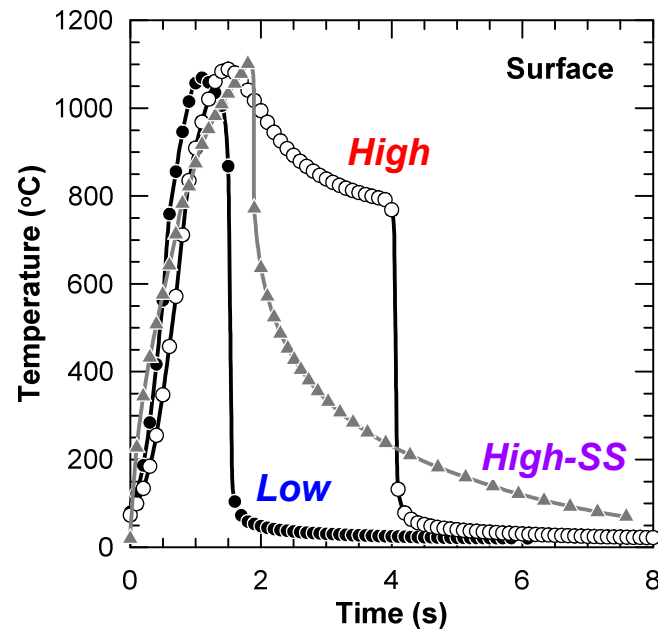
## Processing Parameters for Torsional Fatigue Samples

	Low	High	High-SS
Power (kW)	72	72	128
Frequency (kHz)	196	196	31
Scan Rate (mm/s)	22.9	17.3	---
UCON A Conc. (%)	6	6	2
Flow Rate (L/min)	75	75	173
Eff. Case Depth (%)	25	44	44



# Simulation of Induction Hardening

## Thermal Profiles for Gleeble Testing

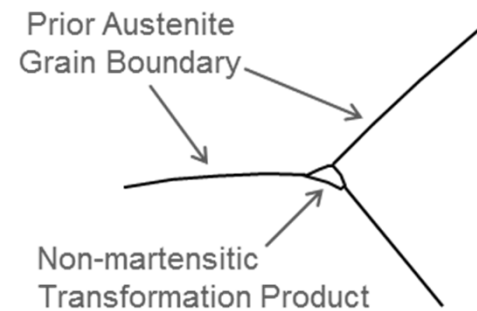
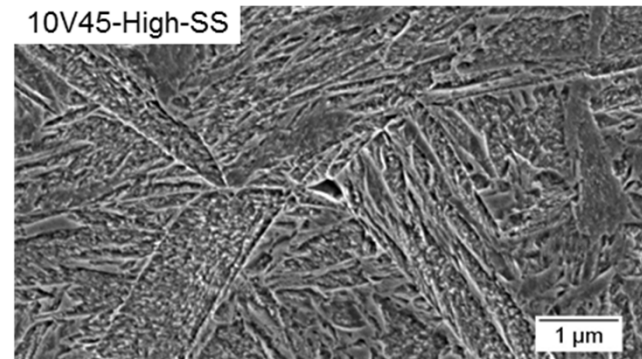
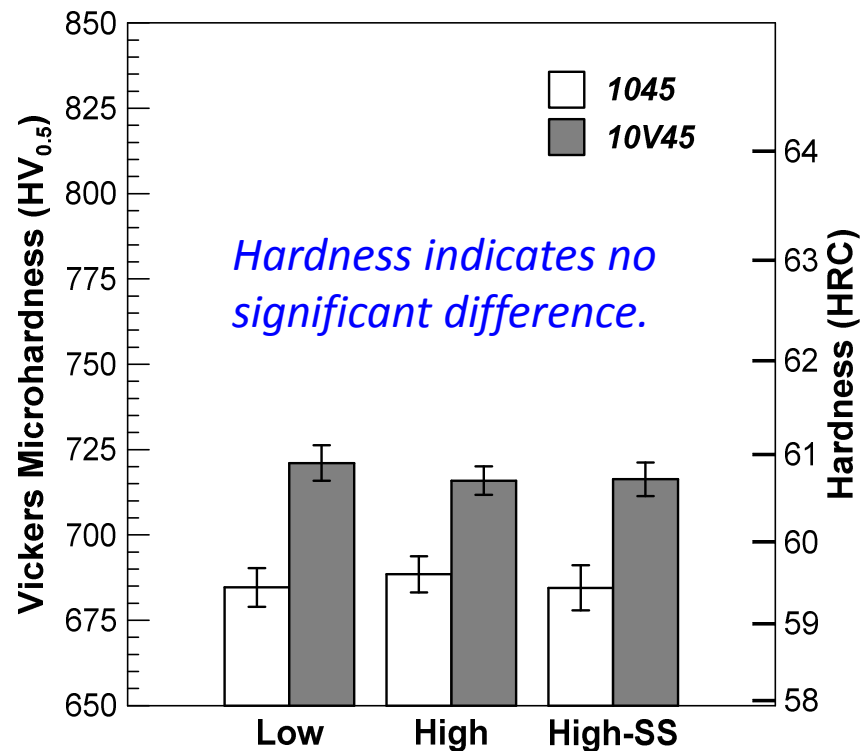


Condition	Software	Location Description	Distance from Surface (mm)
Low	Flux 2D	Surface	---
		Total Case Depth	2.10
High	Flux 2D	Surface	---
		Total Case Depth	3.80
High-SS	ELTA	Surface	---
		Total Case Depth	3.80



# Simulation of Induction Hardening

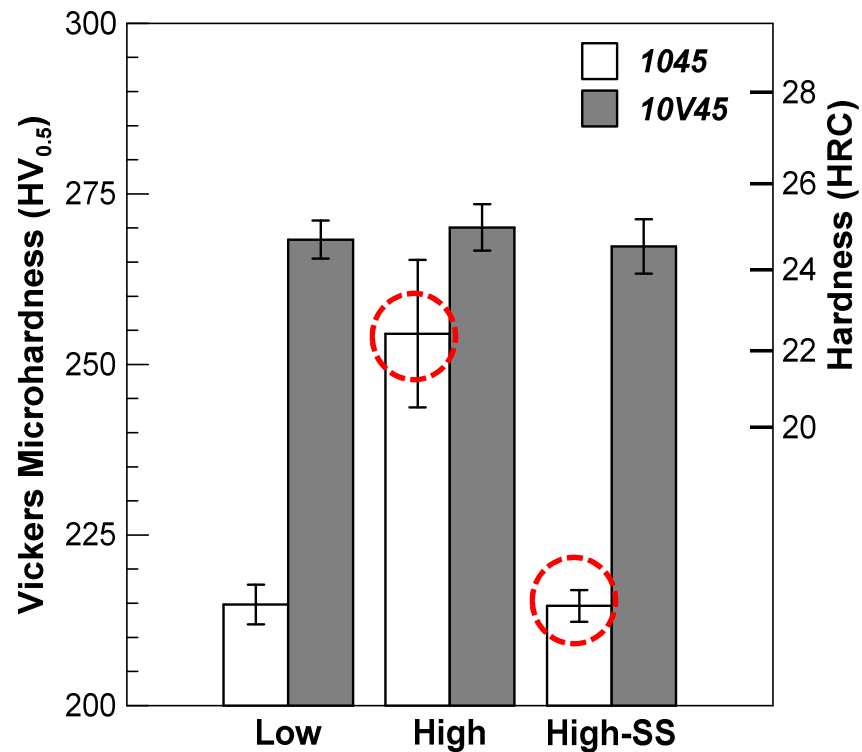
## Gleeble Testing Results – Surface



**<1%**

# Simulation of Induction Hardening

*Gleeble Testing Results – Total Case Depth*

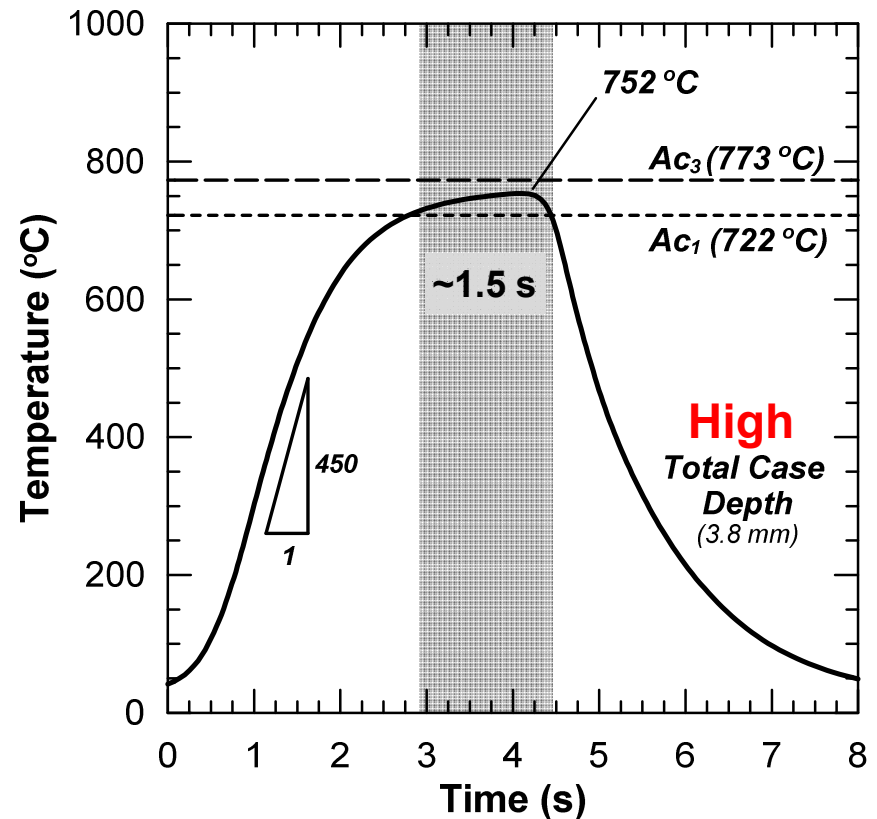
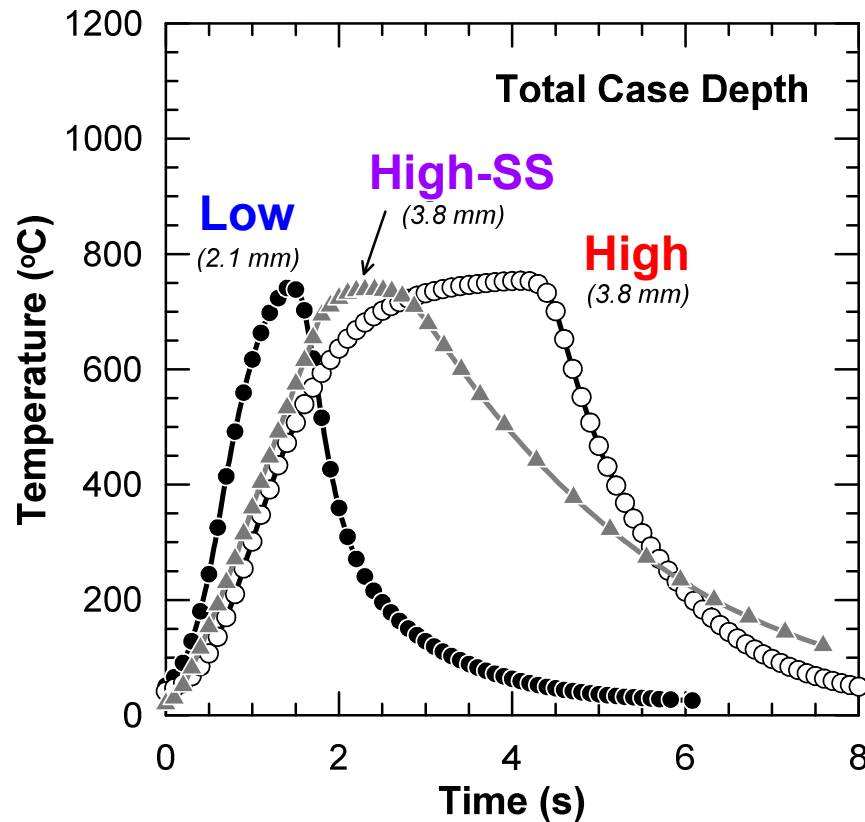


*Significant difference between the 1045 High and High-SS conditions.*

# Simulation of Induction Hardening

15

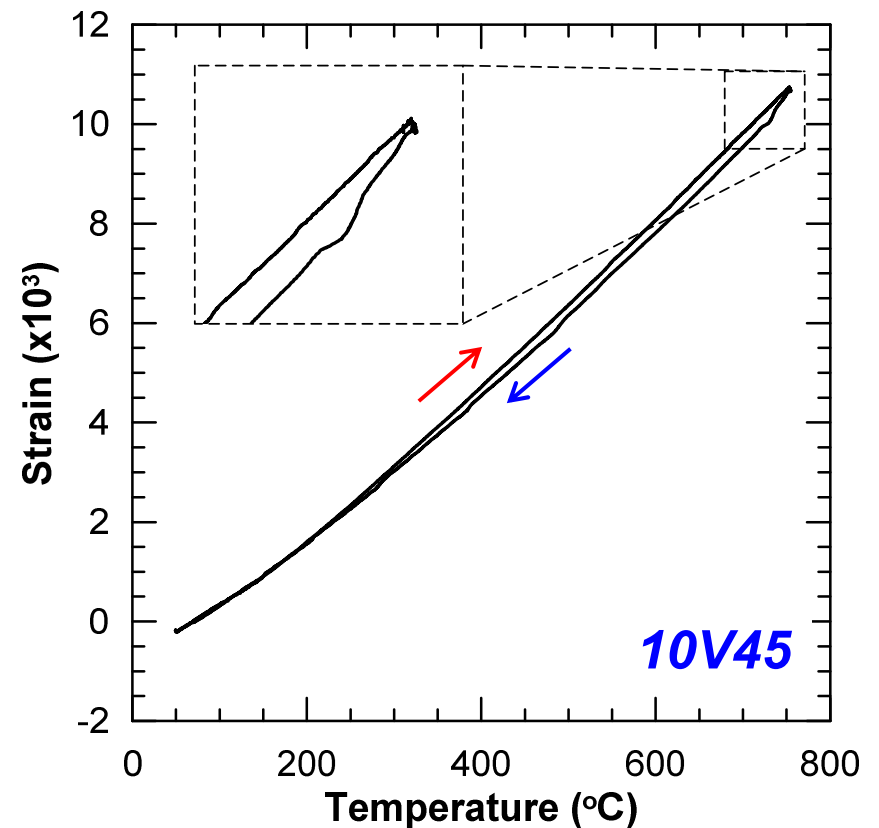
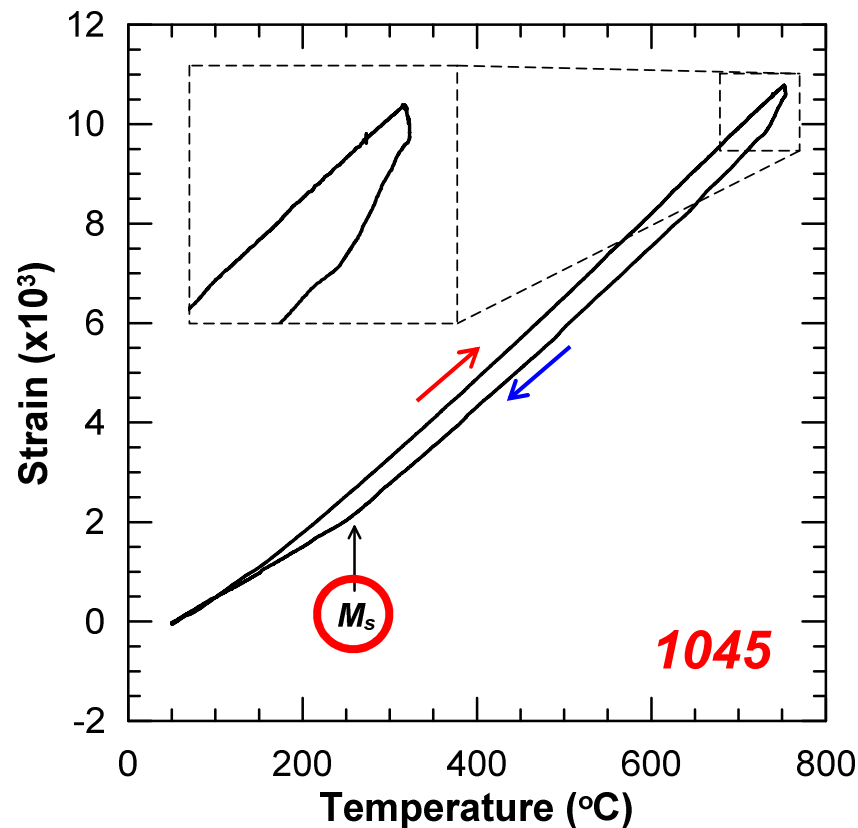
## Gleeble Testing Results – Total Case Depth



# Simulation of Induction Hardening

16

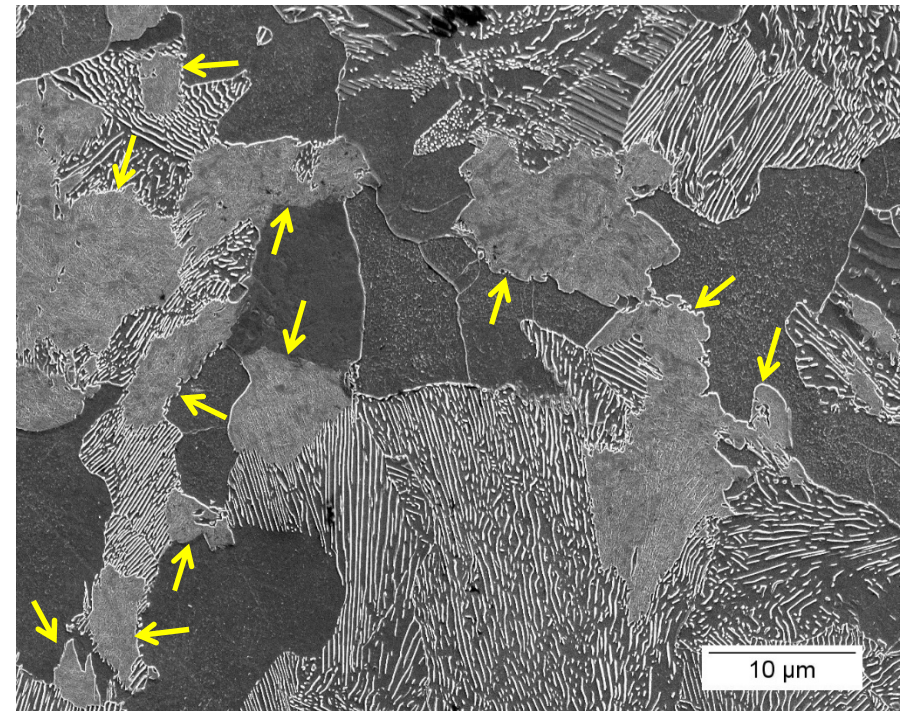
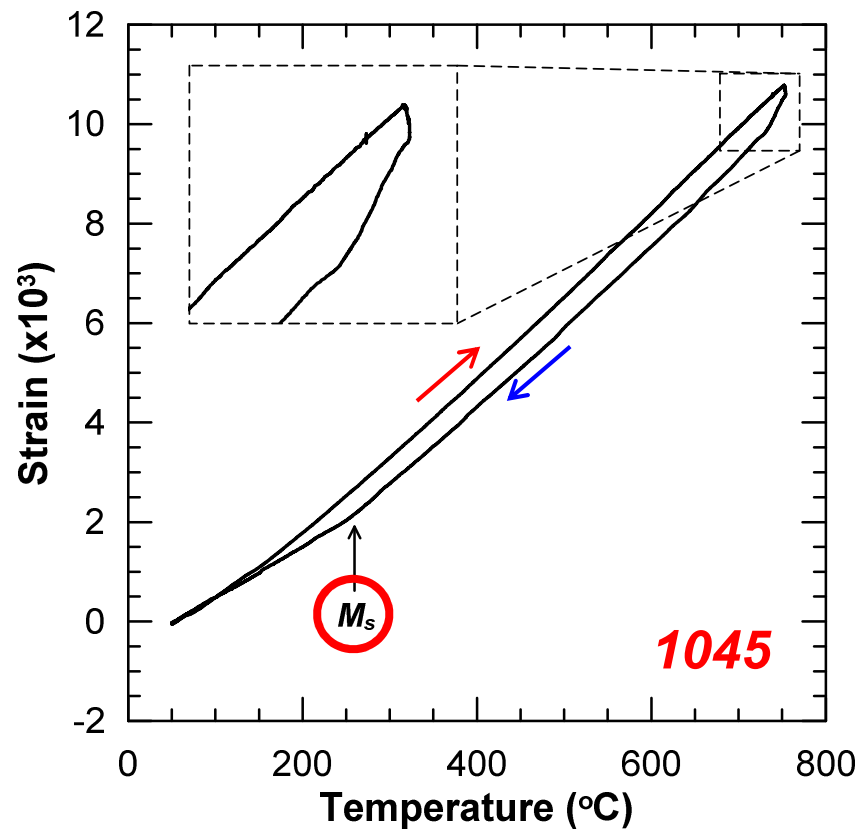
*Gleeble Testing Results – Total Case Depth for High Condition*





# Simulation of Induction Hardening

*Gleeble Testing Results – Total Case Depth for High Condition*

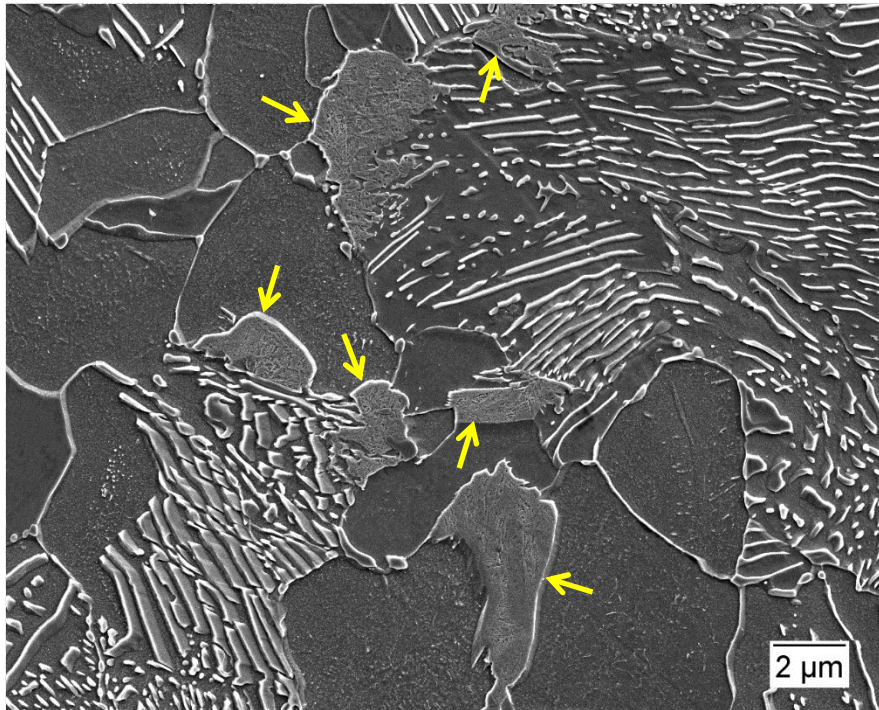


**13.5  $\pm$  0.6 pct**

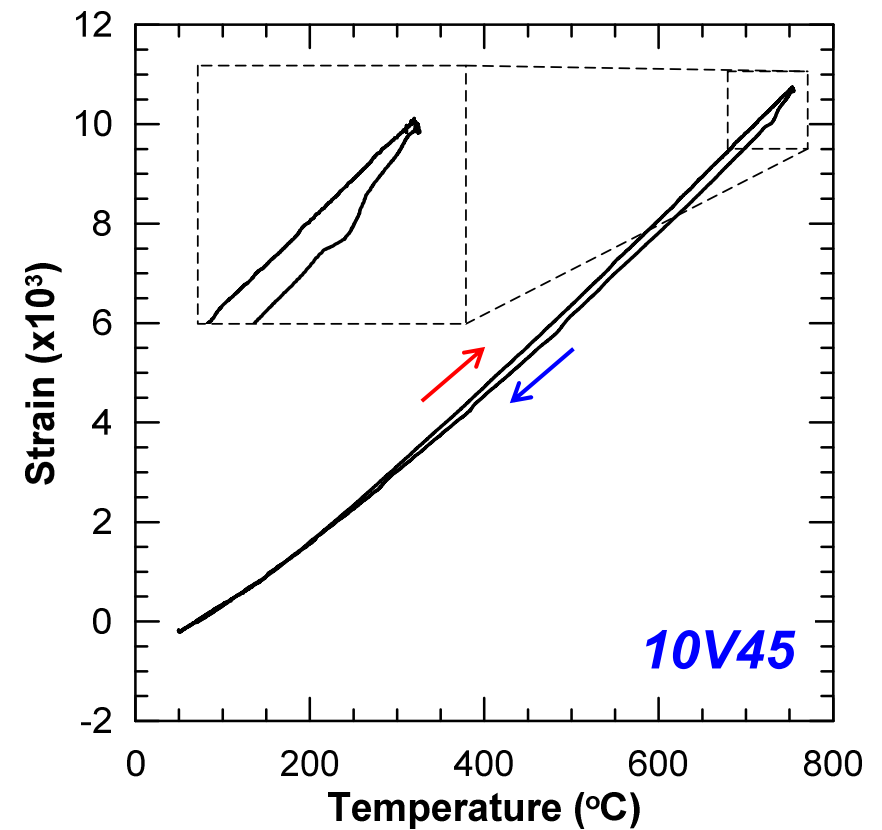
# Simulation of Induction Hardening

18

*Gleeble Testing Results – Total Case Depth for High Condition*



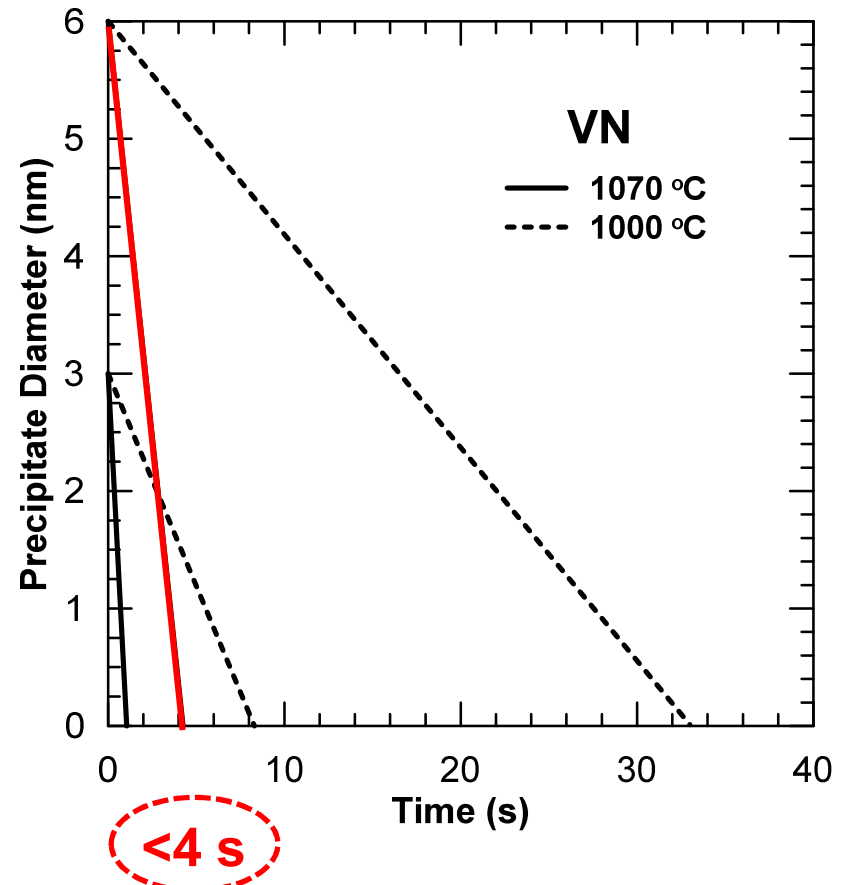
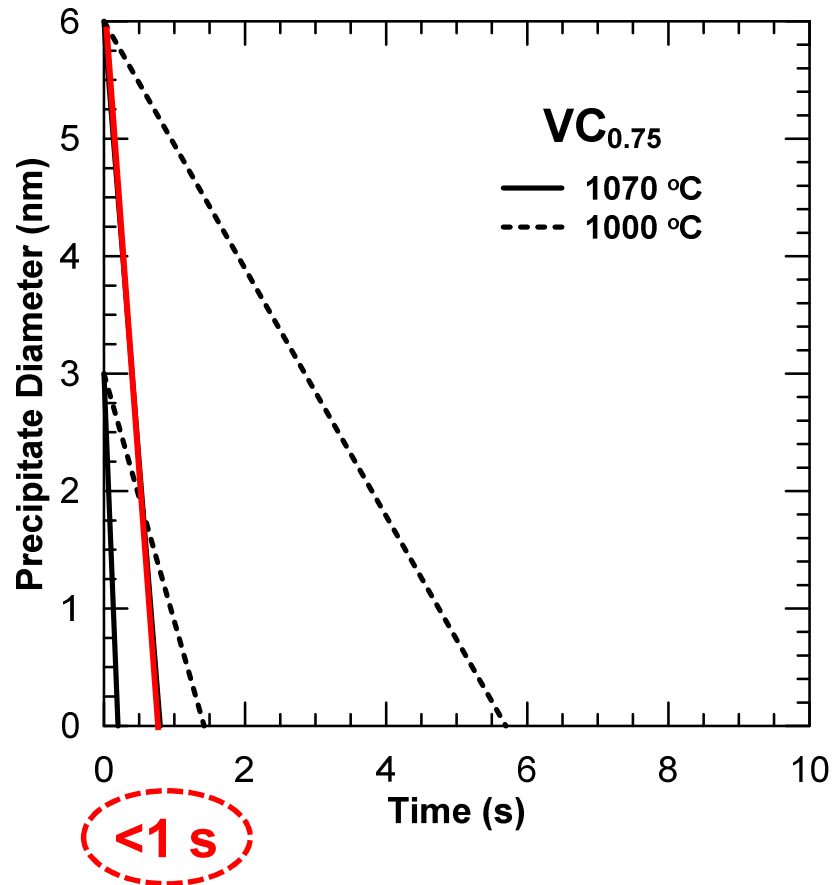
**$1.1 \pm 0.5$  pct**



# Materials

19

## *V(C,N) Precipitate Dissolution*



(Whelan 1969)

## Conclusions

*Microalloying of induction hardened medium carbon steels with vanadium may result in...*

- 1) Increased non-martensitic transformation products in the case.*
- 2) Reduction in total case depth at higher case depths.*

*Lee Rothleutner  
lee.rothleutner@timken.com*